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# Structural Modelling of Expansive Clay Subgrades Treated with Lime

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# PREAMBLE

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In late 2017, Austroads released an updated version of their Guide to Pavement Technology Part 2: Pavement Structural Design.

One new addition to ‘the Guide’ was the introduction of a stabilised subgrade modelling procedure whereby the determination of a suitable treatment thickness and the corresponding design CBR are directly related to the bearing capacity of the underlying subgrade.



# AGENDA

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1. Background
2. Austroads Structural Design Method
3. Austroads Mix Design Method
4. Design Example

# 1

## BACKGROUND



# Expansive Soils in Australia





# Pavement Design

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- ☐ Wetting and drying of expansive soils provides considerable challenges
- ☐ Very thick and expensive pavement structures often required
- ☐ Even with adequate cover, expansive soils can still affect the performance of new pavements



# Effects of Expansive Soils

## PAVEMENT DESIGN (PRELIMINARY)

|           |                     |
|-----------|---------------------|
| ROADS     | - ROAD 6            |
| CLASS     | - COLLECTOR         |
| ESA's     | - $2.0 \times 10^5$ |
| SURFACE   | - 35mm AC           |
| CBR 80    | - 125mm             |
| CBR 45    | - 100mm             |
| CBR 15    | - 245mm             |
| TOTAL BOX | - 505mm             |

ASSUMED CBR 3 SUBGRADE PRIOR TO  
TESTING





# BACKGROUND – AGPT2

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- 4<sup>TH</sup> Edition was published Oct 2017.
- Released Dec 2017.
- State Road Authorities commenced releasing their Pavement Design Supplements from 2018.





# 2

## AUSTROADS STRUCTURAL DESIGN METHOD



# Design Subgrade CBR v Stabilisation Thickness

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The Austroads Guide to Pavement Technology, Part 2: Pavement Structural Design (2017), provides guidance to practitioners on methods for the selection and design of stabilised subgrade materials to improve the California Bearing Ratio (CBR) of the treated layer.

It is a tiered approach with iterations between design CBR and stabilisation thickness.



# STABILISED SUBGRADE DESIGN CBR SELECTION

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Minimum CBR of:

- A. 15%;
- B. Field Results or Presumptive Values;
- C.

$$\text{CBR}_{\text{STAB. SUBGRADE}} = \text{CBR}_{\text{UNDERLYING MATERIAL}} \times 2^{(\text{STABILISED SUBGRADE THICKNESS} / 150)}$$

This approach did not exist in previous design guides



# GOVERNING APPROACH.....*usually*



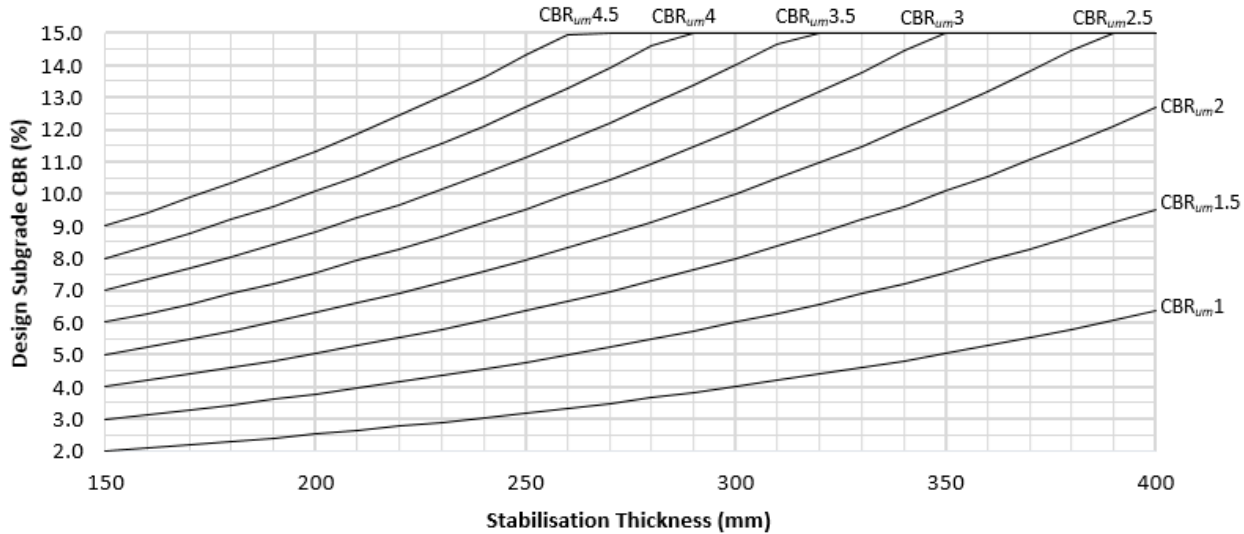
$$\text{CBR}_{\text{STAB. SUBGRADE}} = \text{CBR}_{\text{UNDERLYING MATERIAL}} \times 2^{\left( \frac{\text{STABILISED SUBGRADE THICKNESS}}{150} \right)}$$

The following chart illustrates an iterative approach to selection of a design subgrade CBR and stabilisation thickness based on the above equation.



# STABILISED SUBGRADE DESIGN

## Selection of Design CBR for Stabilised Subgrades





# Mechanistic LEA Properties



Once a design subgrade CBR has been selected, a vertical modulus ( $E_v$ ) is established using the equation below for input into layered elastic analysis models (Austroads, 2017).

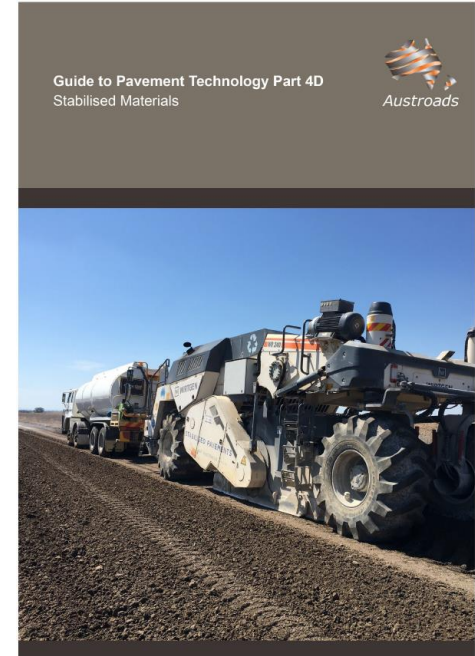
$$\text{Modulus (MPa)} = 10 \times \text{CBR}$$

A maximum value of 150MPa is normally adopted with a Poisson's ratio of:

- 0.45 for cohesive materials
- 0.35 for non-cohesive materials.

# 3

## AUSTROADS MIX DESIGN METHOD





# BINDER SELECTION



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| Particle size                                      | More than 25% passing 75 µm sieve |                      |                      | Less than 25% passing 75 µm sieve                               |                  |                      |
|--|-----------------------------------|----------------------|----------------------|---|------------------|----------------------|
| Plasticity index (PI)                              | $PI \leq 10$                      | $10 < PI < 20$       | $PI \geq 20$         | $PI \leq 6$<br>& $PI \times$<br>% passing<br>$75 \mu m \leq 60$ | $PI \leq 10$     | $PI > 10$            |
| <b>Binder type</b>                                 |                                   |                      |                      |   |                  |                      |
| Cement and cementitious blends <sup>(1,3)</sup>    | Usually suitable                  | Doubtful             | Usually not suitable | Usually suitable  | Usually suitable | Usually suitable     |
| Lime   | Doubtful                          | Usually suitable     | Usually suitable     | Usually not suitable  | Doubtful         | Usually suitable     |
| Bitumen  | Doubtful                          | Doubtful             | Usually not suitable | Usually suitable  | Usually suitable | Usually not suitable |
| Bitumen/ lime blends                               | Usually suitable                  | Doubtful             | Usually not suitable | Usually suitable  | Usually suitable | Doubtful             |
| Granular   | Usually suitable                  | Usually not suitable | Usually not suitable | Usually suitable  | Usually suitable | Doubtful             |
| Dry powder polymers                                | Usually suitable                  | Usually suitable     | Usually unsuitable   | Usually suitable  | Usually suitable | Usually not suitable |
| Other proprietary chemical products <sup>(2)</sup> | Usually not suitable              | Usually suitable     | Usually suitable     | Usually not suitable  | Doubtful         | Usually suitable     |





# Hydrated Lime v Quicklime

|   | Hydrated Lime, $\text{Ca(OH)}_2$ | Quicklime, $\text{CaO}$ |
|---|----------------------------------|-------------------------|
| Composition                             | $\text{Ca(OH)}_2$                | $\text{CaO}$            |
| Form                                    | Fine powder                      | Granular                |
| Equivalent $\text{Ca(OH)}_2$ /unit mass | 1.00                             | 1.32                    |
| Bulk Density ( $\text{t/m}^3$ )         | 0.45 to 0.56                     | 1.05                    |
| Used in Laboratory                      | Yes                              | No                      |
| Used in Construction                    | Yes (least common)               | Yes (most common)       |

Lime slurry and agricultural lime are not used for conventional road stabilisation projects in Australia



# Quicklime Conversion



If quicklime is specified for use in the field, a conversion factor 0.76 is applied to the laboratory determined hydrated lime application rate.

$$\text{Quicklime (\% in field)} = \text{Hydrated Lime (\% in lab)} \times 0.76$$

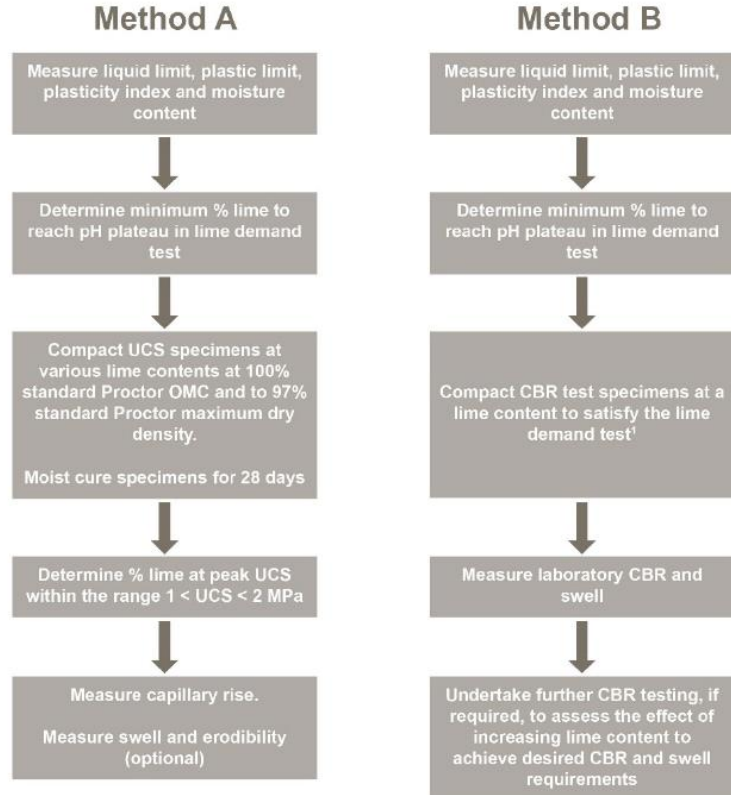
Eg. If the lab determined application rate is 4% H/L by mass,

The field application rate can be: 3% Q/L by mass.



# Mix Design Methods

Figure 4.4: Determination of lime content of earthworks materials



- ❑ Method A is traditionally only used by QLD DTMR
- ❑ Method B is the most common approach for local government



# Lime Demand Testing

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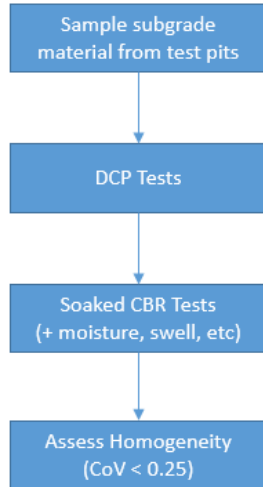


- ❑ Measures the pH of the clay at various lime contents.
- ❑ Lime demand value characterised as the minimum lime content to satisfy cation exchange by reaching a pH of 12.4 (Little, 1995).
- ❑ Lime application rates for CBR testing are recommended to be at LD, LD+1% and LD+2% as a minimum testing regime.
- ❑ Confirmation of a design application rate is then determined by selecting the lime content where the CBR exceeds the design CBR by a factor of 2 to account for variations in host material and lime properties.

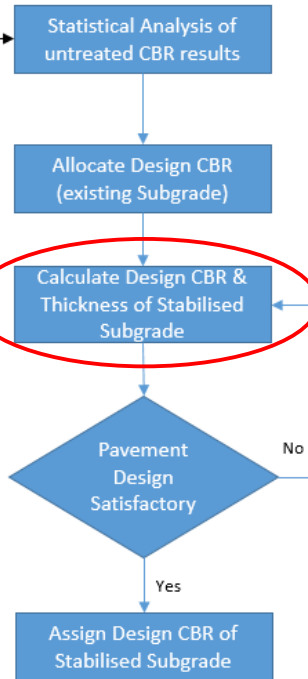


# Simplified Design Summary

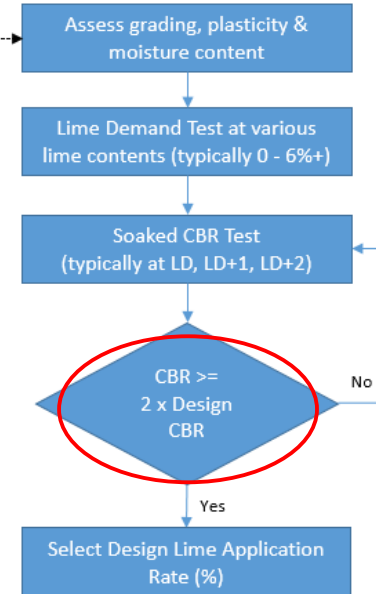
## Geotechnical Investigation



## Structural Design



## Mix Design







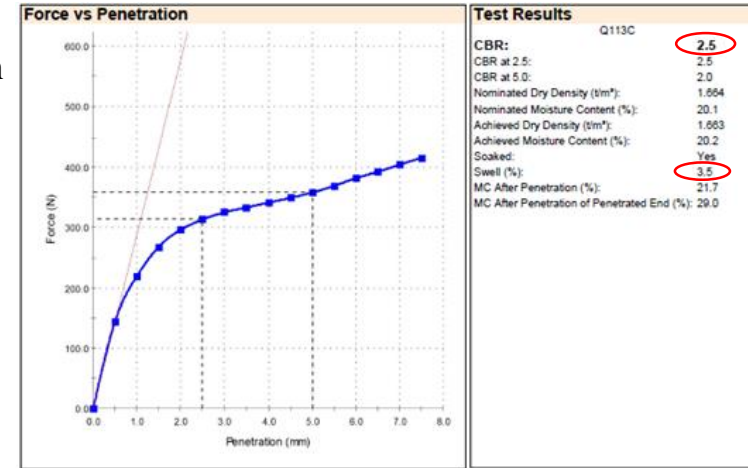
# Design Example

A Consultant needs to design a pavement for a new subdivision development. The following design parameters have been assigned:

- Traffic loading: 9.0E+05 DESA
- Existing expansive clay subgrade: CBR2.5 (3.5% swell)

Table 5.2: Guide to classification of expansive soils

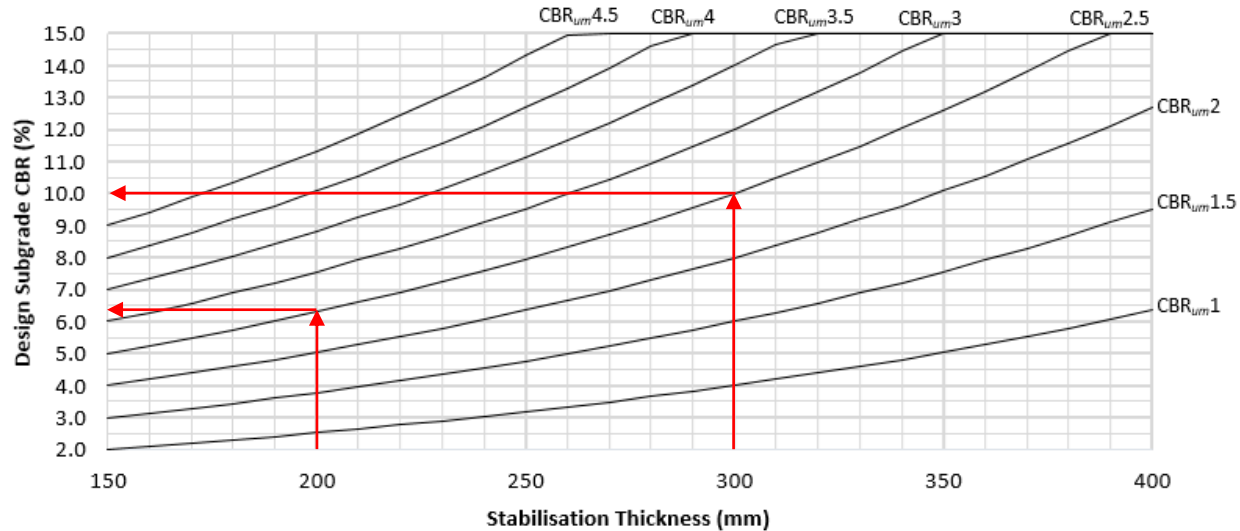
| Expansive nature | Liquid limit (%) | Plasticity Index | PI x % < 0.425 mm | Swell (%) <sup>(1)</sup> |
|------------------|------------------|------------------|-------------------|--------------------------|
| Very high        | > 70             | > 45             | > 3200            | > 5.0                    |
| High             | > 70             | > 45             | 2200–3200         | 2.5–5.0                  |
| Moderate         | 50–70            | 25–45            | 1200–2200         | 0.5–2.5                  |
| Low              | < 50             | < 25             | < 1200            | < 0.5                    |





# Stabilised Subgrade

## Selection of Design CBR for Stabilised Subgrades



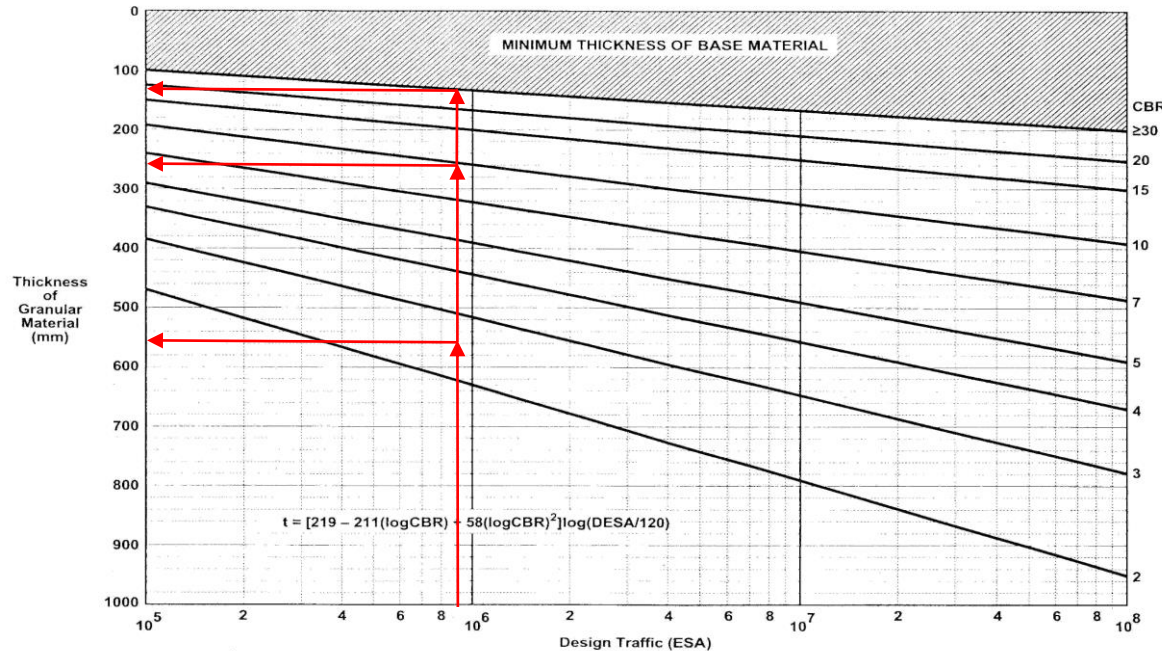
The maximum allowable design CBR is:

- 10% for a 300mm treatment
- 6% for a 200mm treatment





# Pavement Layer Thickness Determination



Minimum total cover over expansive clay subgrade CBR2.5 = 560mm

Minimum cover over 300mm  
Stabilised Subgrade CBR10 = 260mm

Minimum thickness of granular base  
CBR80 = 140mm

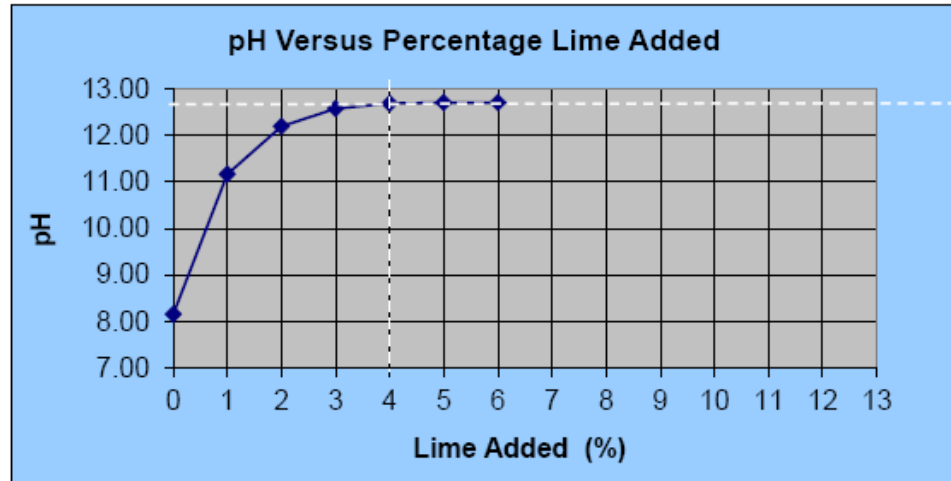
Balance thickness for granular  
subbase CBR30 = 120mm  
(260 – 140)

Figure 8.4 Design chart for granular pavements with thin bituminous surfacing



## Step 2: Mix Design

LIME DEMAND :  % (Hydrated Lime)

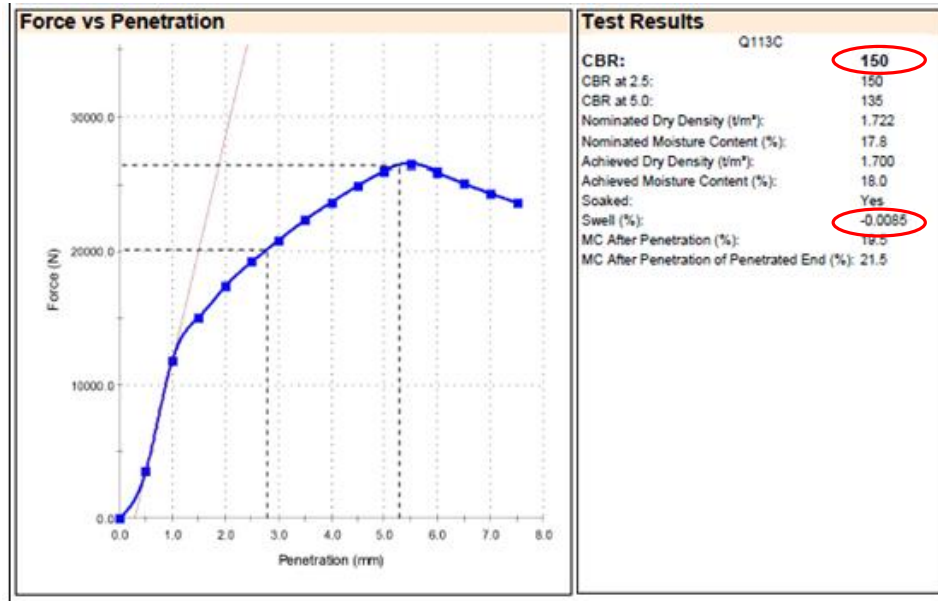


Lime demand testing resulted in LD=4%.



## Step 2: Mix Design

CBR testing was carried out at LD=4% which resulted in CBR=150% and no Swell





# Design Recommendation

As the CBR test result at LD (4%) exceeded the target strength of CBR20 (design CBR10 x 2), the final design is:

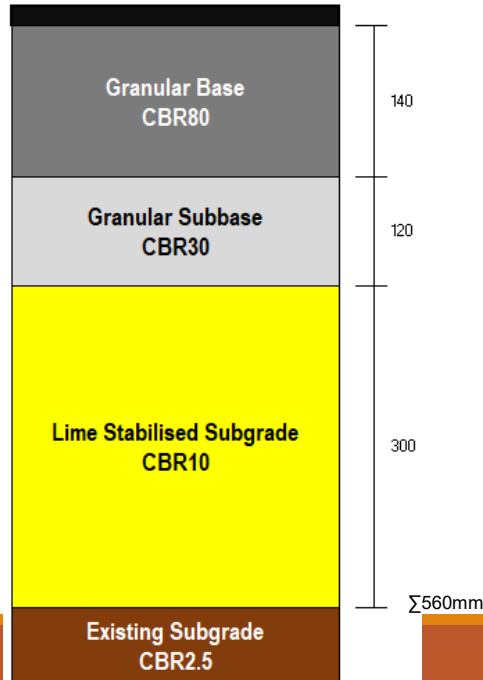
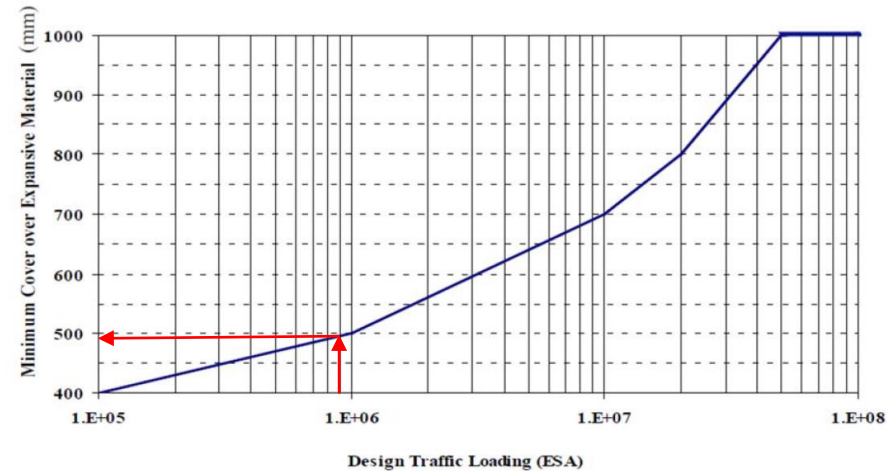


Figure 5.1 – Minimum Cover over Expansive Material



# 5



## SUMMARY



# KEY TAKEAWAYS

- Lime stabilisation can be extremely effective to limit permanent deformation and reduce the overlying pavement thickness, as long as proper design methods are followed
- Revised 2017 Austroads Structural Design Guide
- Design CBR increases of approximately 200-400%.
- Stabilised Subgrade Design Approach

$$\text{CBR}_{\text{STAB. SUBGRADE}} = \text{CBR}_{\text{UNDERLYING MATERIAL}} \times 2^{\left(\frac{\text{STABILISED SUBGRADE THICKNESS}}{150}\right)}$$



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